

Aachen, 25.09.2014, 4. AMAP Kolloquium

Joining challenges in automotive lightweight applications

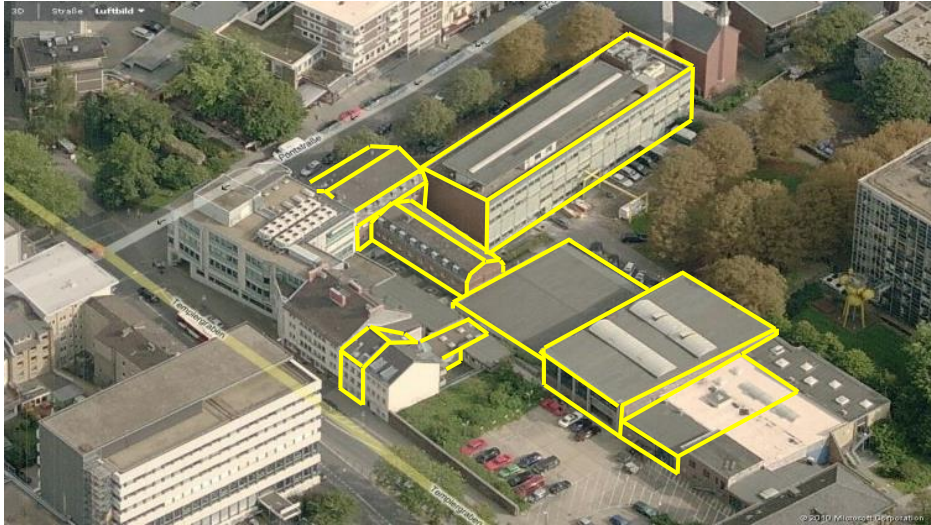
Uwe Reisgen

Christoph Geffers

- Introduction
- Motivation
- Lightweight design and multi-material mix
- Challenges to joining technology
- Composite design and multi-material mix in production
- Summary

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Univ.-Prof. Dr.-Ing. U. Reisgen
- Head of Institute -

Employees:

- 30 scientific staff
- 25 non-scientific staff
- 5 trainees
- 40 student assistants

Budget:

- ca. 4.5 million €
(80 % third party funds)

Space for tests and laboratory :

- ca. 2700 qm

Teaching:

- Welding and Joining Technology for Bachelor und Master students
- International welding engineer (IWE)



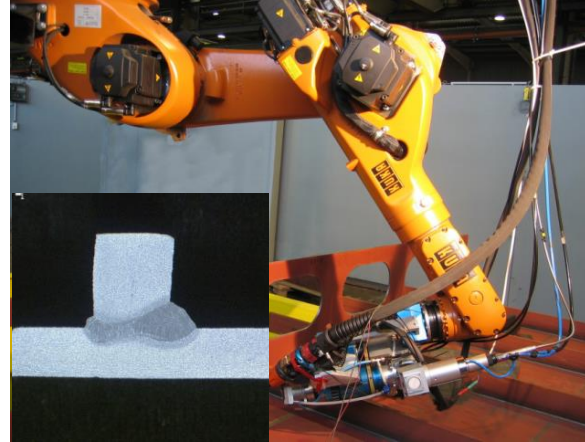
- **Arc Welding**

- Gas Metal Arc Welding
- TIG-, Plasma-, SA-Welding
- Surfacing
- Robotic/Sensoric



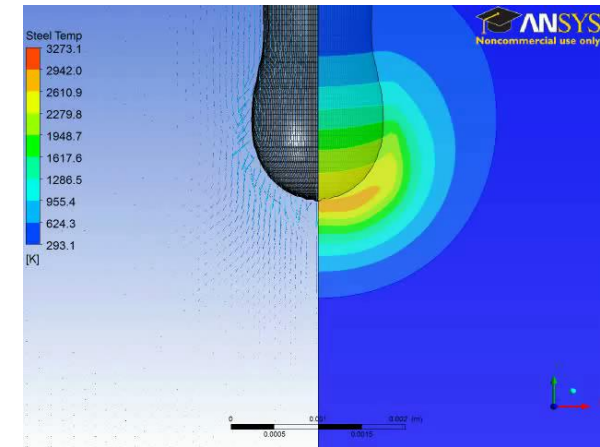
- **Beam Welding**

- Laser Beam Welding
- Electron Beam Welding
- Health and Work Safety

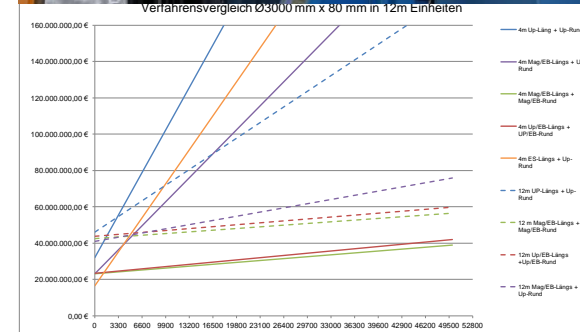


- **Cold Technologies**

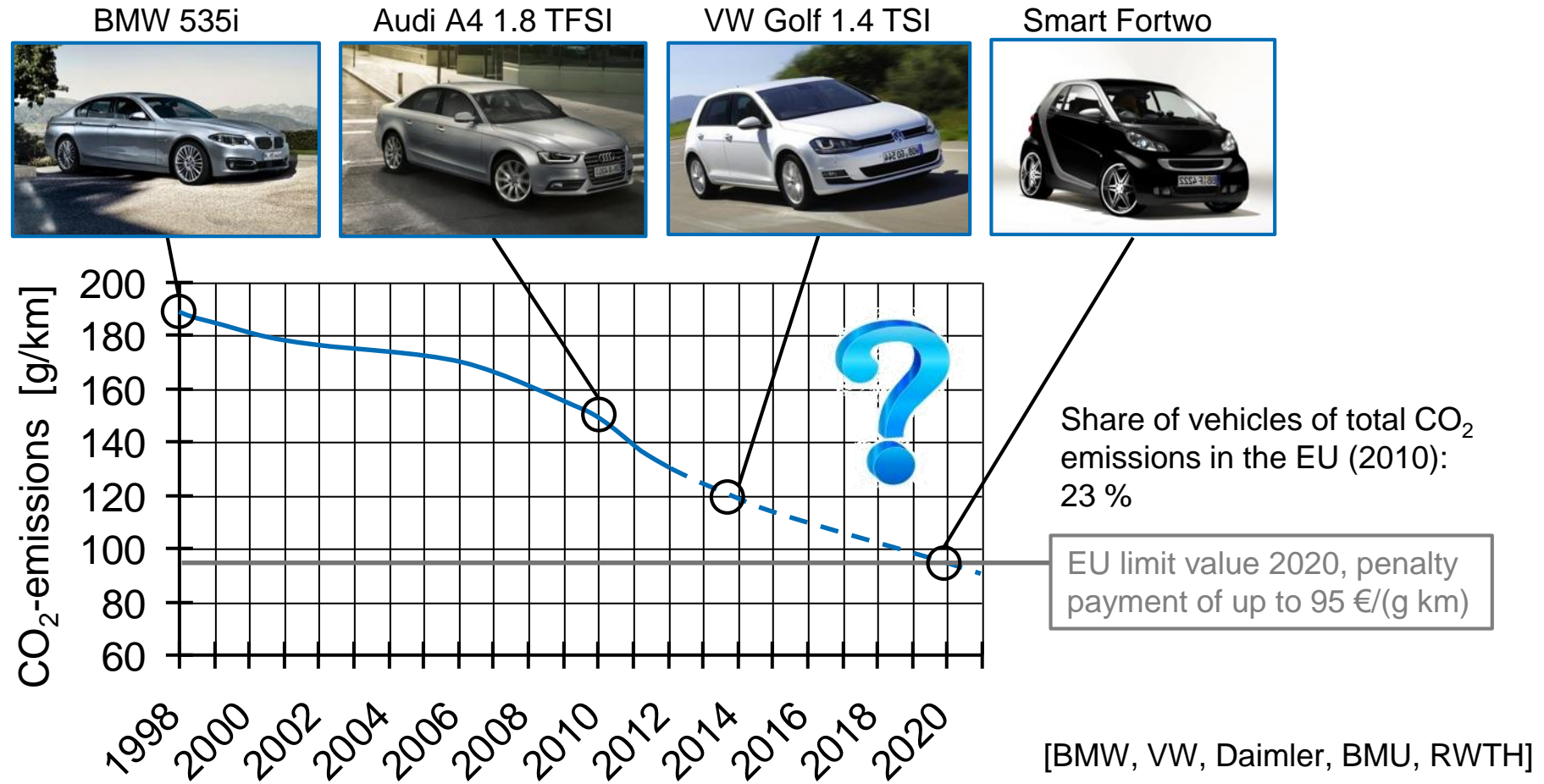
- Adhesive Bonding
- Resistance Welding
- Friction Stir Welding
- Ultrasonic Welding
- Simulation and Modelling

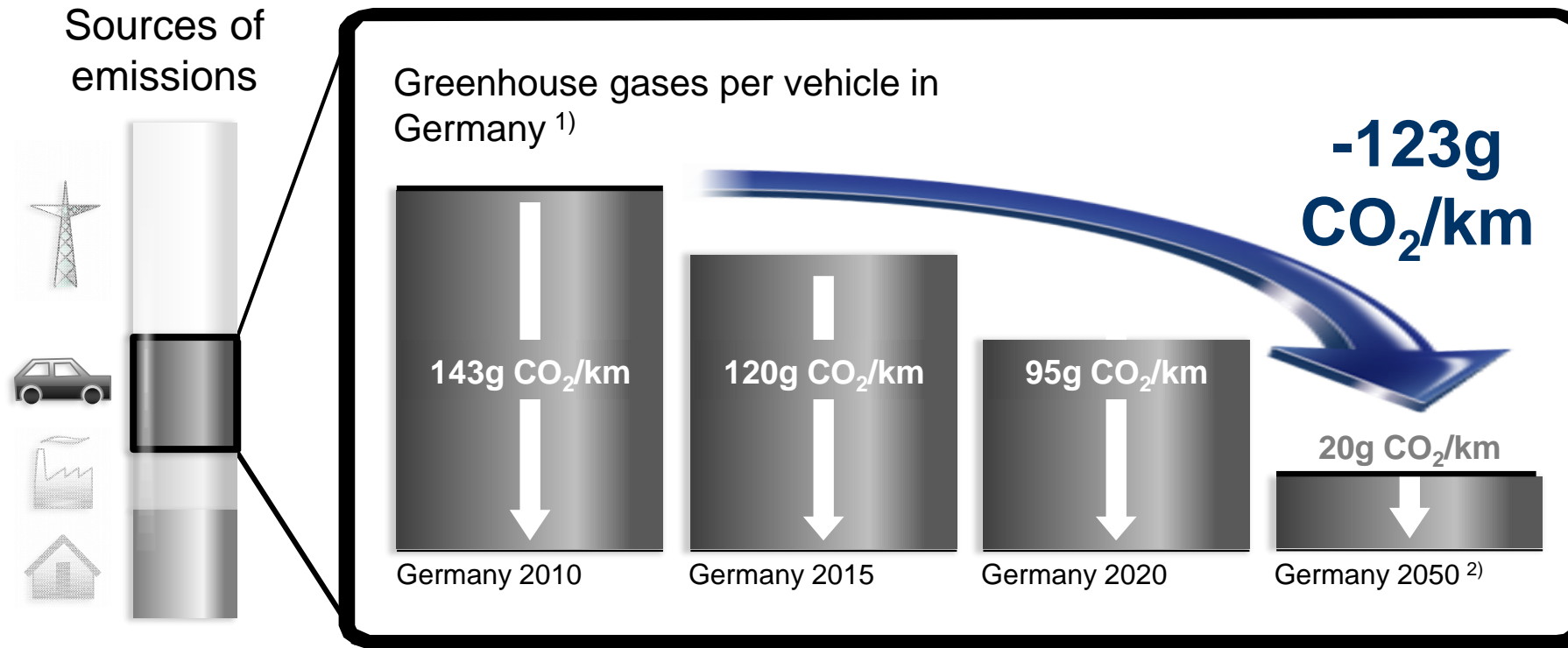


- Analysis of welding processes and optimization
- Development of cost-efficient welding processes and implementation
 - Consulting by our specialists
 - Consideration of requirements and needs of the client
 - The total manufacturing chain is considered
 - Only what the client needs
- Support for automation tasks
- Technology support on-site
 - During commissioning
 - During production
 - “Emergency services“
- Work-Shops
- Prototypes and pre-series
- Support in the search for competent system suppliers



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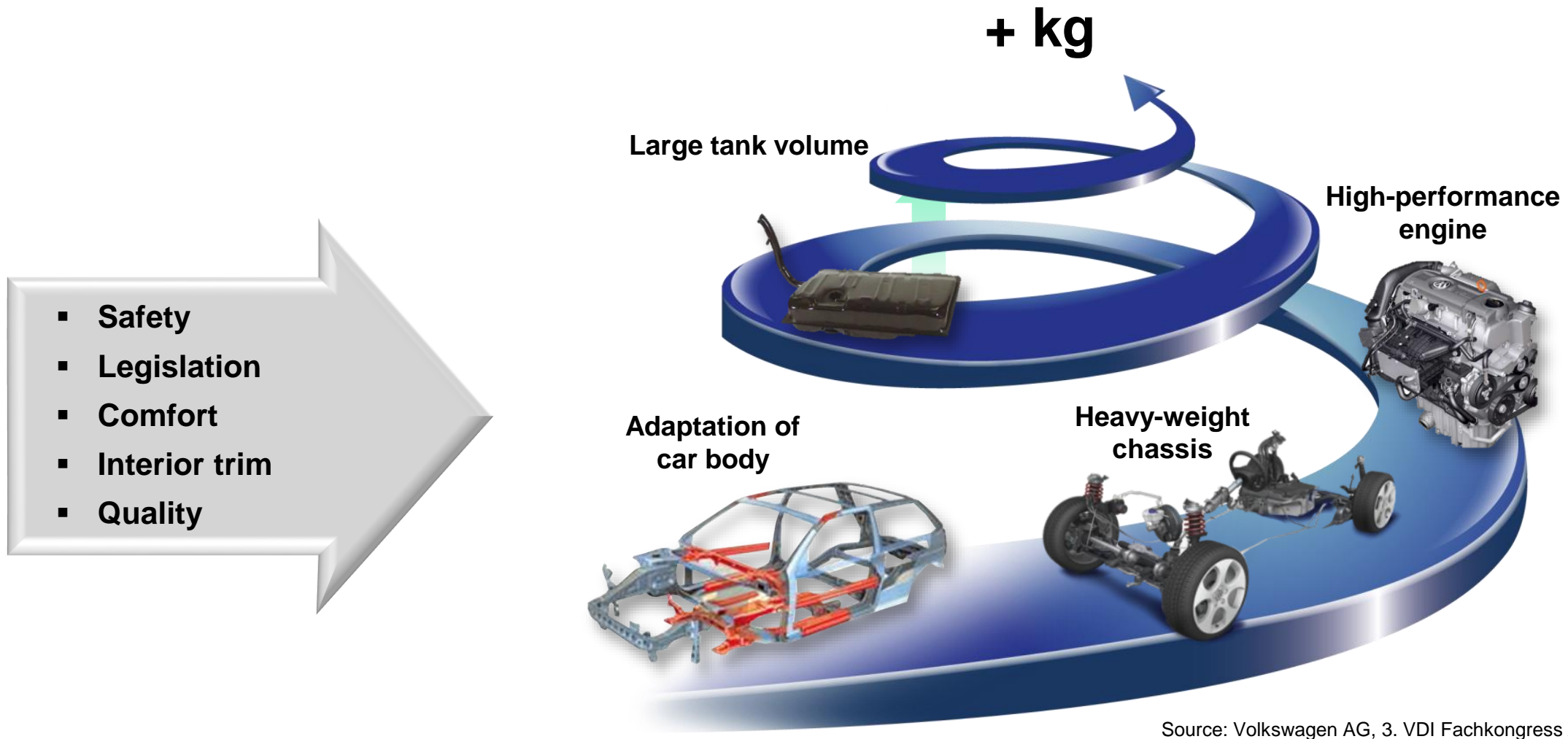




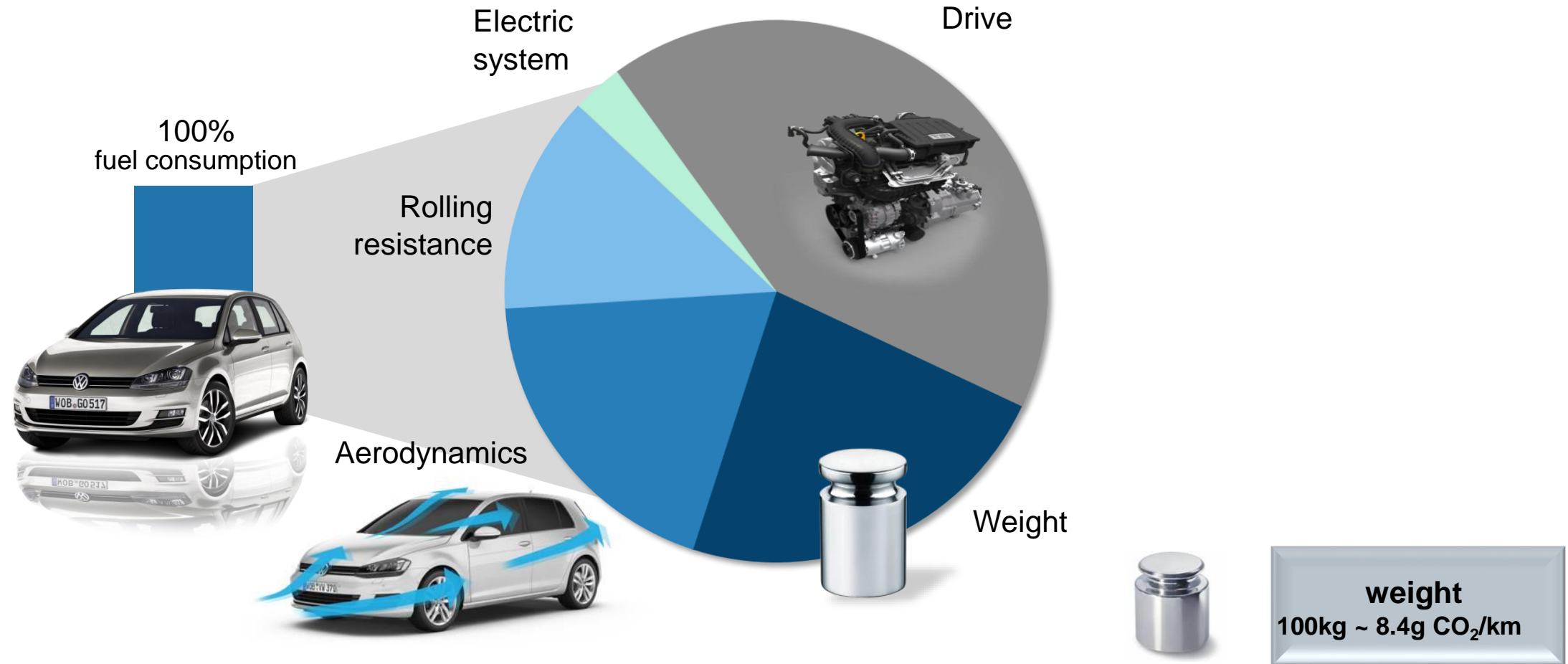
1) Source: McKinsey & Company, Ministry for the Environment

2) Memorandum of understanding, e.g. EU and G8+5 states, part of Copenhagen Accord 2009

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Source: Volkswagen AG, 3. VDI Fachkongress 2013



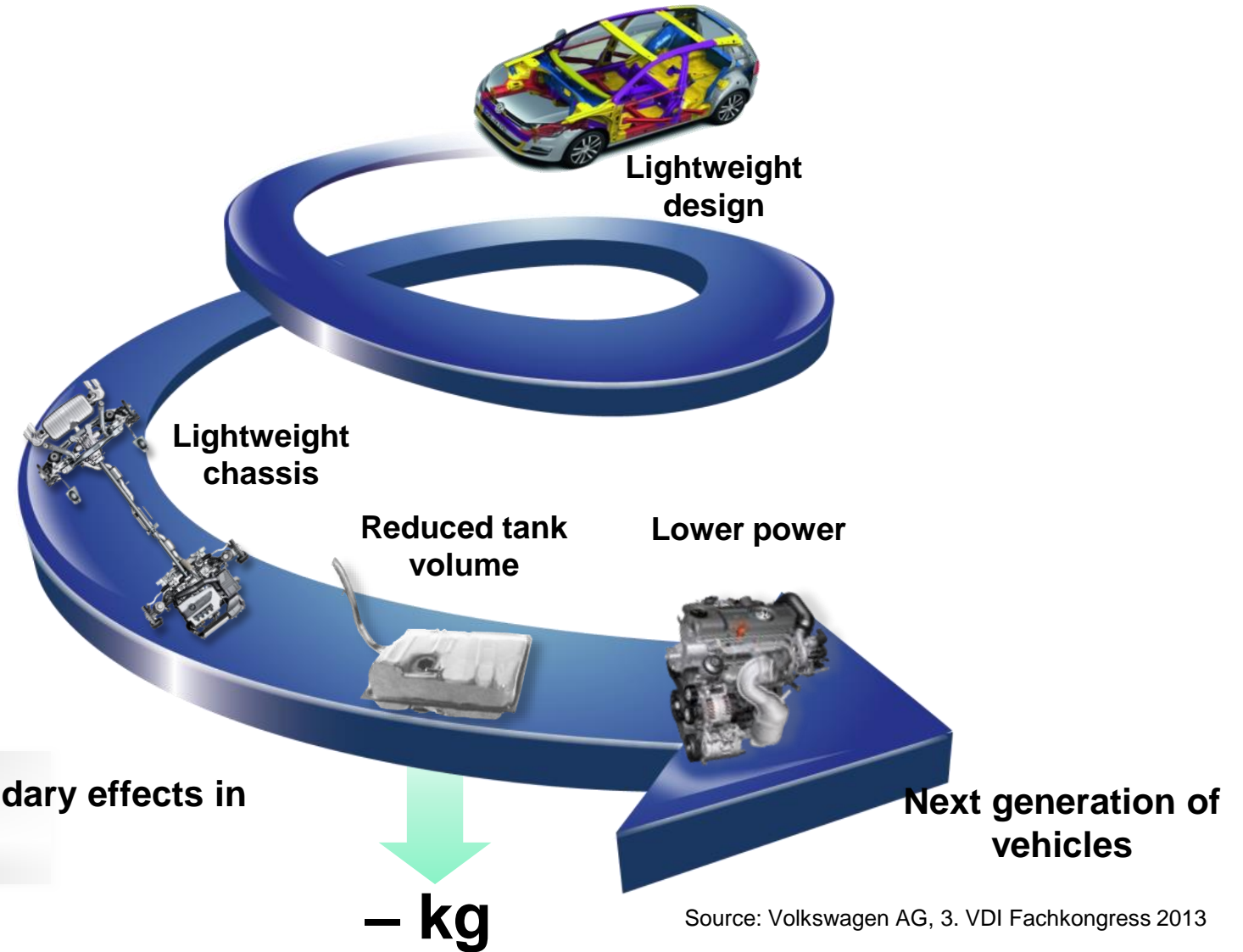
Source: Volkswagen AG, Automotive Lightweighting & Manufacturing 2014

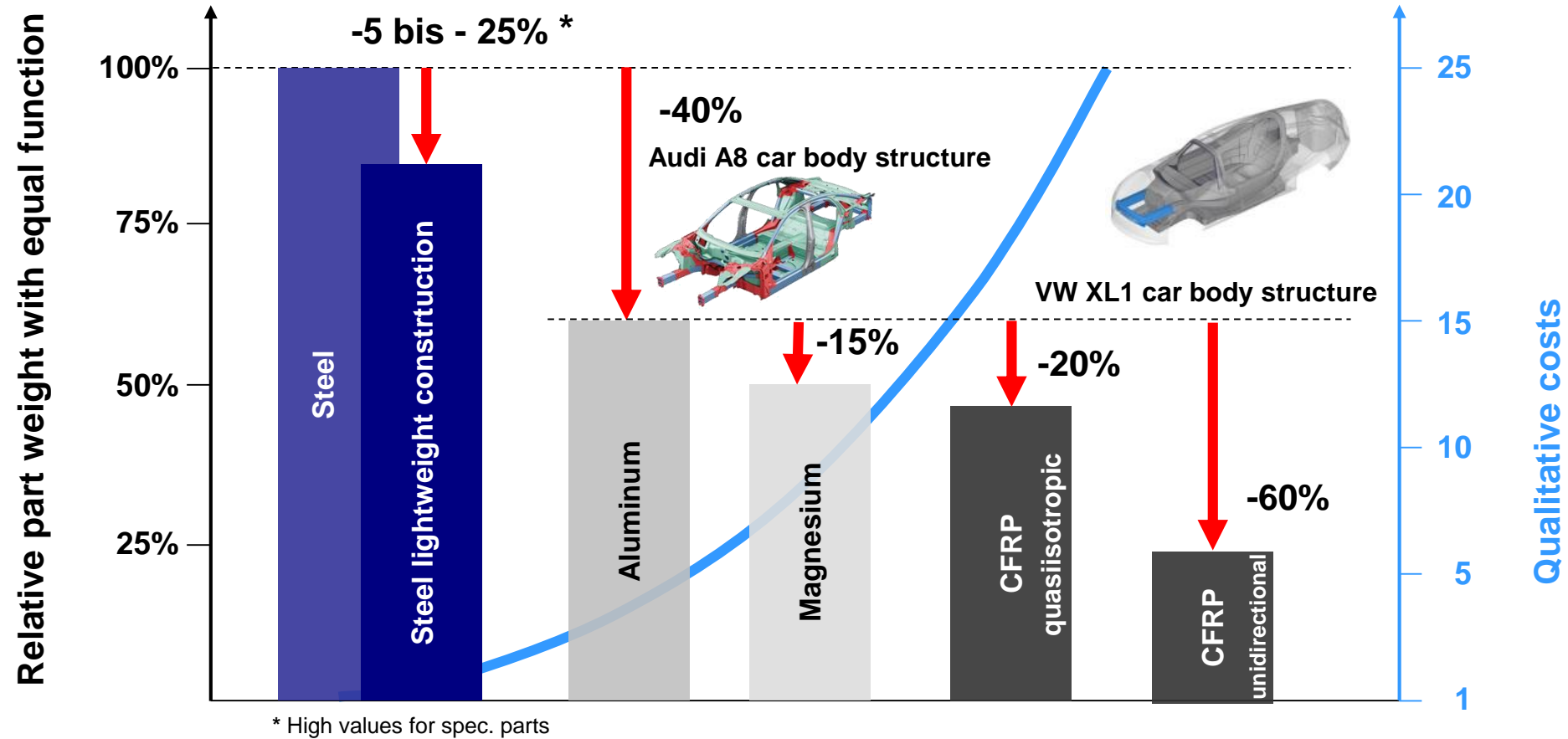
Almost 1/4 of consumption are a direct consequence of the weight

- Part- and function integration
- New materials and processes
- Cost - /weight optimization



Starting with the car body allows secondary effects in the entire vehicle





Sheet monocoque design (steel)



Audi-Space-Frame (ASF) design



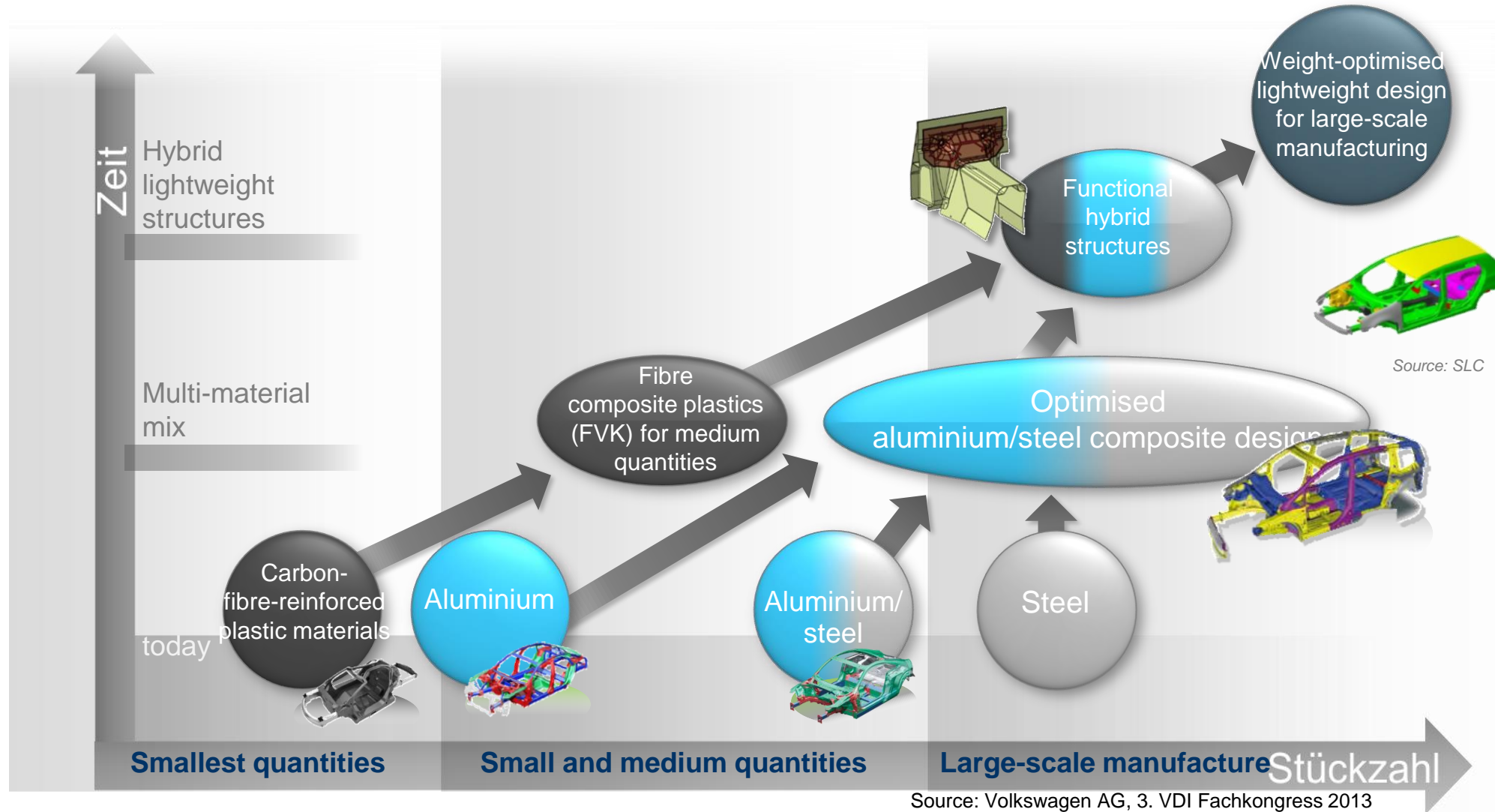
Composite design (e.g. ASF® car body with steel rear part)

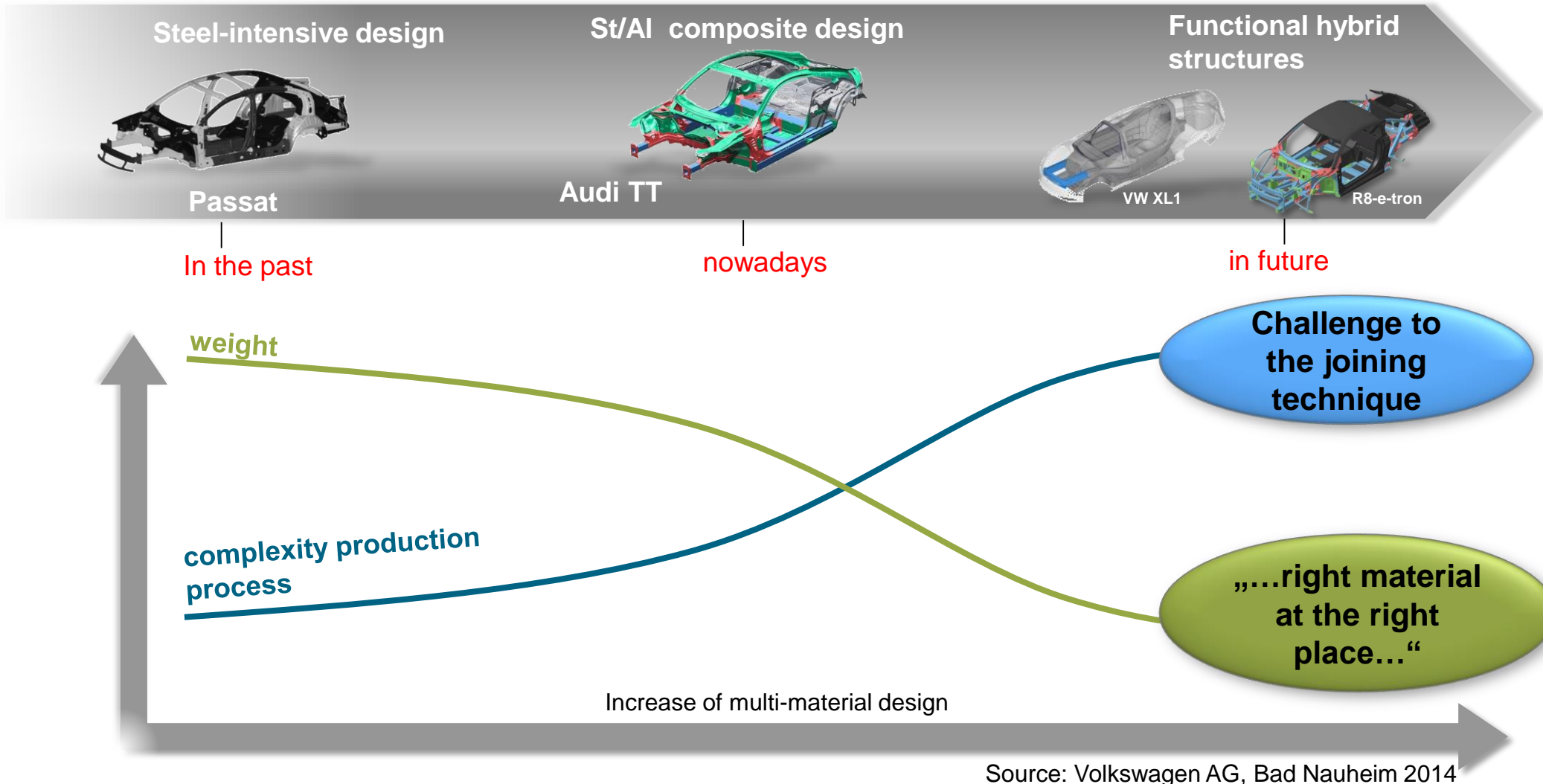


CFRP design



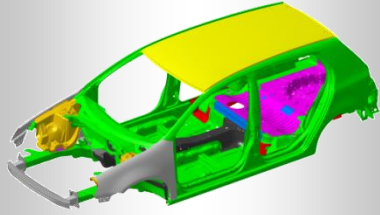
Source: Volkswagen AG, Werkstoffsymposium 2012
„Prozess- und Werkstoffinnovationen in der Pulvermetallurgie“





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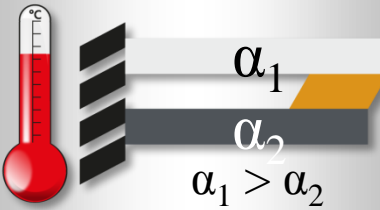
Application



Future car body design concepts with composite design

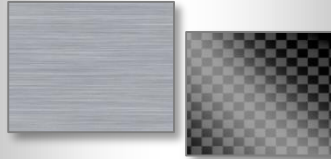
- Thermal load in paintwork drying processes
- Material combination of highest-strength steels/ aluminium / magnesium/fibre-reinforced plastic materials
- Structural crash-proof joints

Challenges



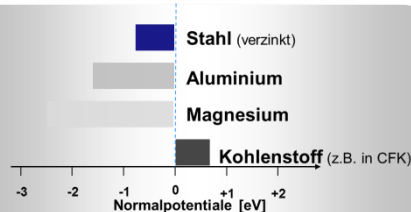
Different heat expansion coefficients

Intermetallic phases in fusion welding processes



New surfacing combinations

(coatings, lubricants, release agents)

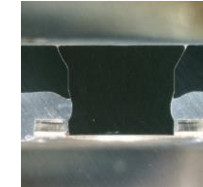
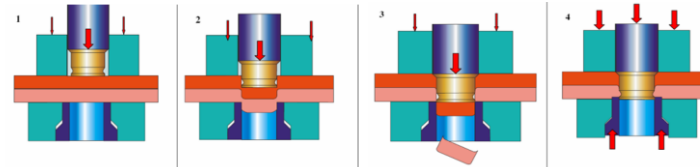


Increased risk of contact corrosion

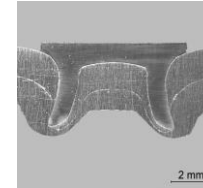
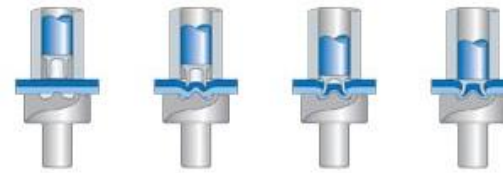
(potential difference aluminium / steel and also aluminium / magnesium fibre-reinforced plastic materials)

Quelle: Volkswagen AG

Rivetting with solid rivet

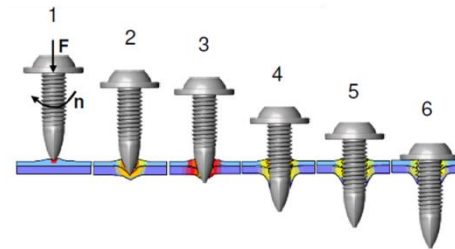


Self pierce rivetting (with semi-tubular rivet)



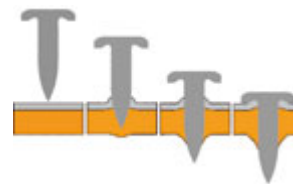
Source: Böllhoff

Flow drill screw (FDS), with/without predrilled hole



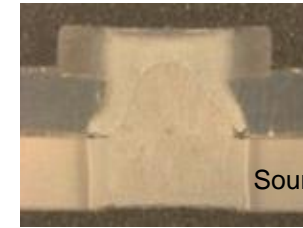
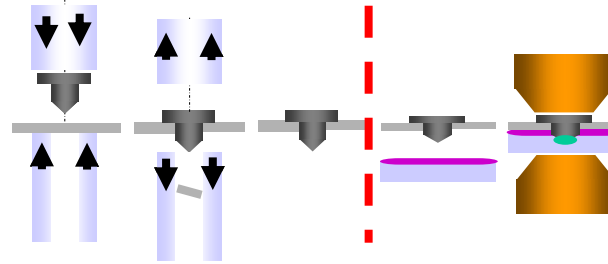
Source:LWF

High-speed stud-setting



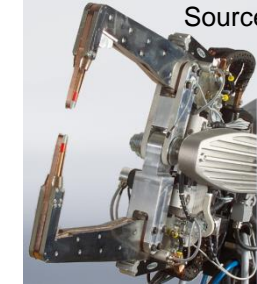
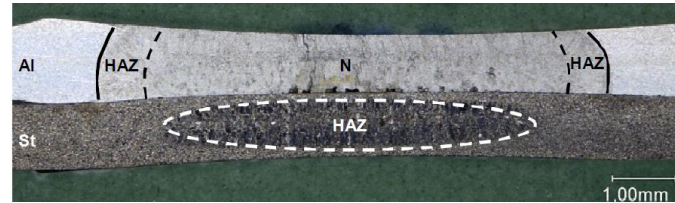
Source:Böllhoff

Resistance element welding



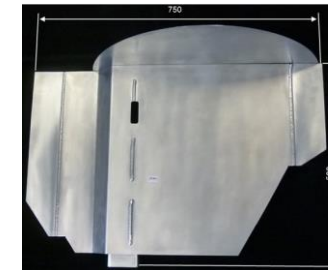
Source: VW

Resistance spot welding via process tapes (DeltaSpot)

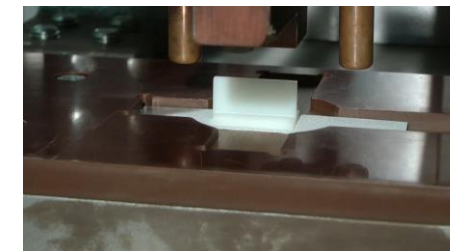


Source: Fronius

CMT braze welding



Thermal direct joining



General Limits of Rivetting:

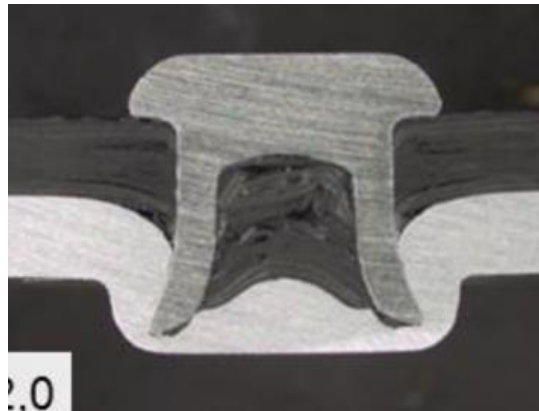
- The quasi-static loads are below the achievable strength values of RP welding
- Two-sided accessibility
- Complementary element required
- A punching develops
- High joining forces (up to 100 kN)- heavy C-guns – large space required



Source: Avdel

Limits of semi-tubular self piercing rivetting compared to solid rivetting:

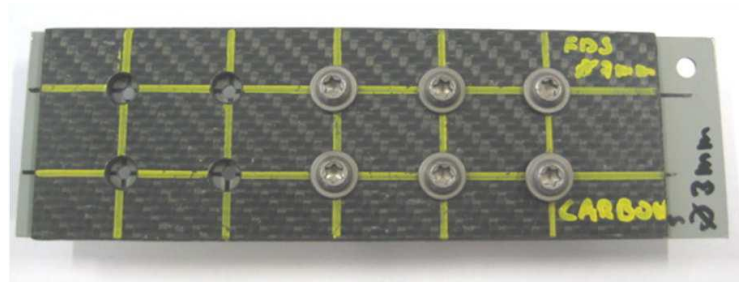
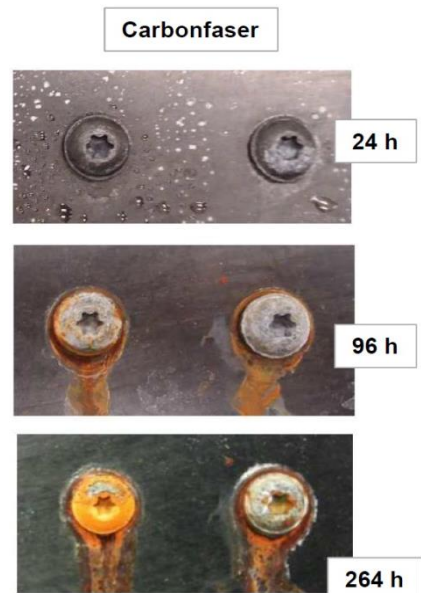
- Sheet strength values only up to max. 1000 MPa instead of 1600 MPa
- Maximally three instead of possibly four sheet layers
- High mechanical load on rivets
- Thicker sheet required on side of die
- It is impossible to join brittle cast materials
- Joining forces of up to 60 kN



Semi-tubular self piercing rivet: Damage of the fibre-reinforced material by squeeze force and process fluctuations
Source: Magna

Limits of FDS:

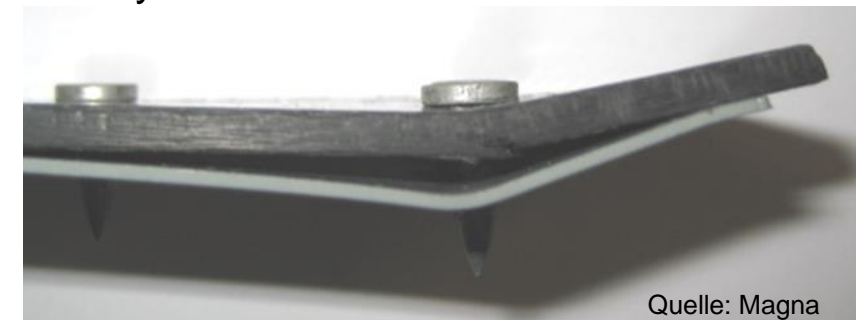
- Local heat flow
- Complementary element required
- Preferably from the thinner into the thicker material
- Preferably to be screwed from the softer into the harder material



Source: Magna

Limits of Stud-Setting:

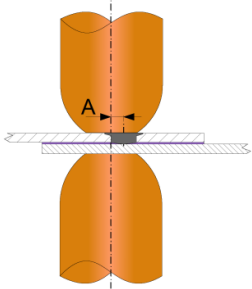
- Joint is undetachable
- Complementary element required
- Loud impulse noises during setting of studs
- Rear sheet layer must offer necessary support
- The material on the side of the setting has a max. strength of approx. 1000 MPa, the rear material can have a strength of approx. 1600 MPa
- Minimum material strength for the rear sheet of 1,5 mm in the case of steel and of 2,5 mm in the case of aluminium
- Material combination: preferably thin into thick and soft into hard



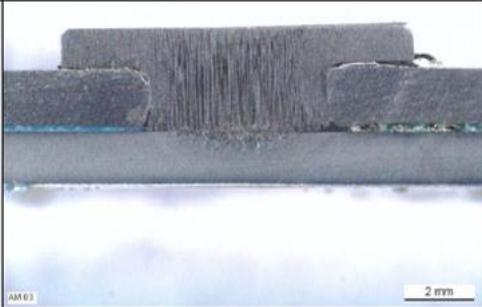
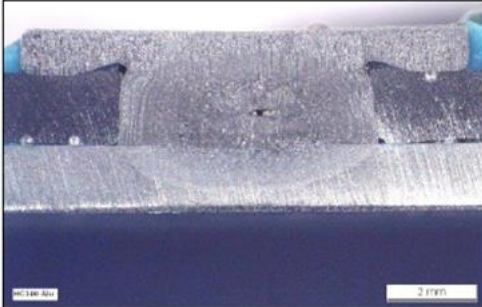
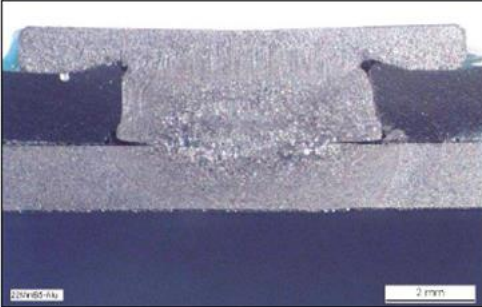
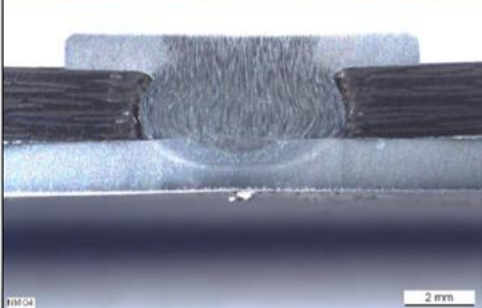

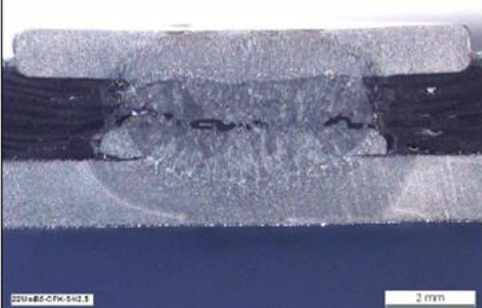
Rivtac: Fracture of the fibre-reinforced structure. Fibre-reinforced material takes in kinetic energy and causes thus the base material to deform too slowly, the consequence is risk of fracture

Limits of resistance element welding (WES):

- Two-sided accessibility
- Complementary element required
- A punching develops
- Handling safety required



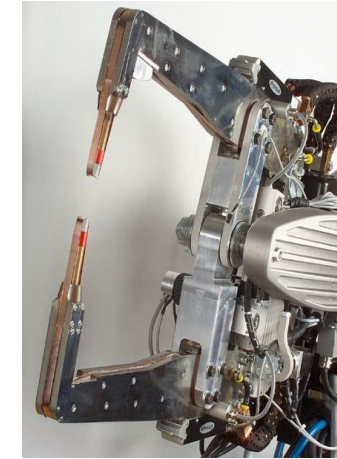
Disturbing influence: Shifting of the electrodes

	HC340LA (1,5 mm)	HC340LA (1,5 mm)	22MnB5 +AlSi (1,5 mm)
EN AW-6016 (1,5 mm)			
PA6.6CF45 (2,0 mm)			
	<p>Schweißzeit: 10 ms Schweißstrom: 6,5 kA</p> <ul style="list-style-type: none"> - Deckbleche thermisch unbeeinflusst - Serientauglichkeit kritisch - Schweißlinse kritisch 	<p>Schweißzeit: 50 ms Schweißstrom: 6,5 kA</p> <ul style="list-style-type: none"> - Randschmelzung am CFK - Linseneindringtiefe kritisch - Bindungsfehler in Schweißlinse - Klebstoffentgasung/-verbrennung 	<p>Schweißzeit: 50 ms Schweißstrom: 6,5 kA</p> <ul style="list-style-type: none"> - Randschmelzung am CFK - Bindungsfehler in Schweißlinse - Klebstoffentgasung/-verbrennung

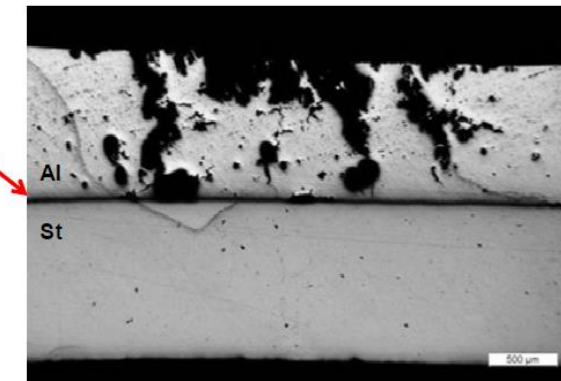
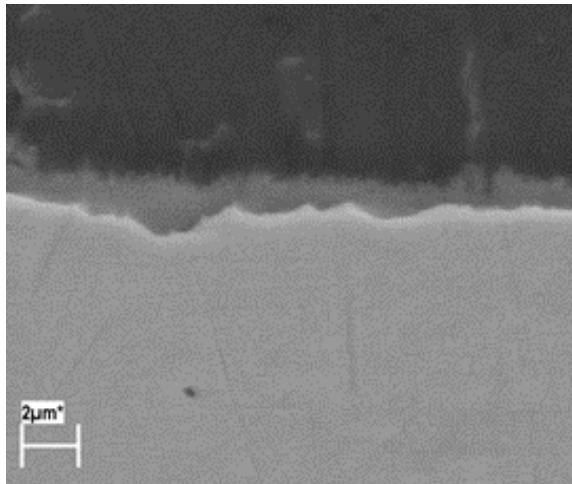
Source: LWF, Paderborn

Limits of DeltaSpot:

- Process tapes required
- Additional expenditure/costs, change of the process tapes
- Restrictions accessibility / flange width by the process tapes
- Process control with aluminium/steel joints in combination with adhesives is still a challenge



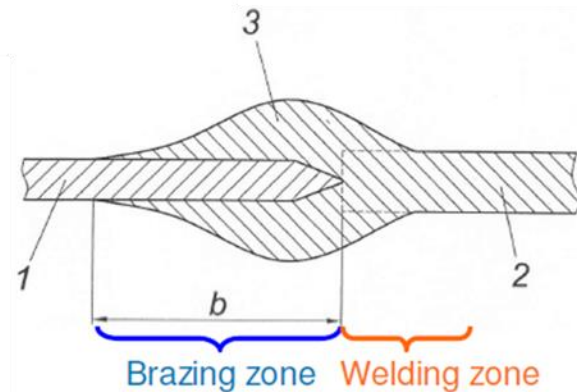
Source: Fronius



Source: Audi, Bad Nauheim 2012

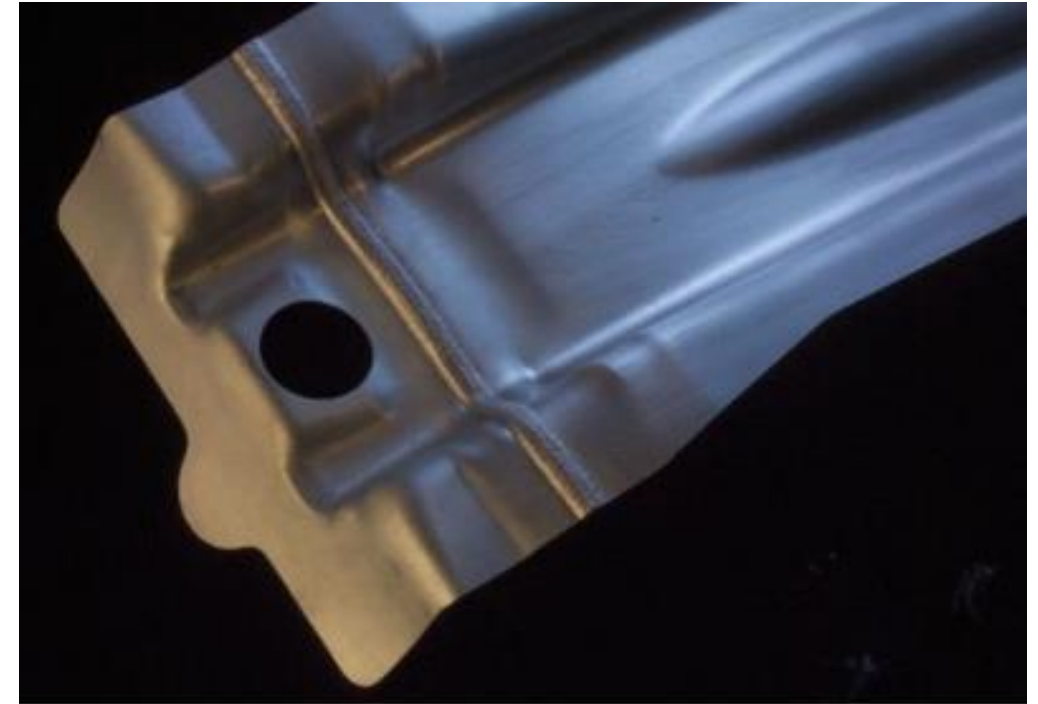
Limits : CMT braze welding of hybrid board by Fronius and Voestalpine

- Only for production of blanks
- Steel sheet side must be galvanized
- Special edge preparation on the steel side
- Weld reinforcement
- Restricted forming property caused by weld reinforcement



1. Steel sheet, galvanised
2. Aluminium sheet
3. Filler material

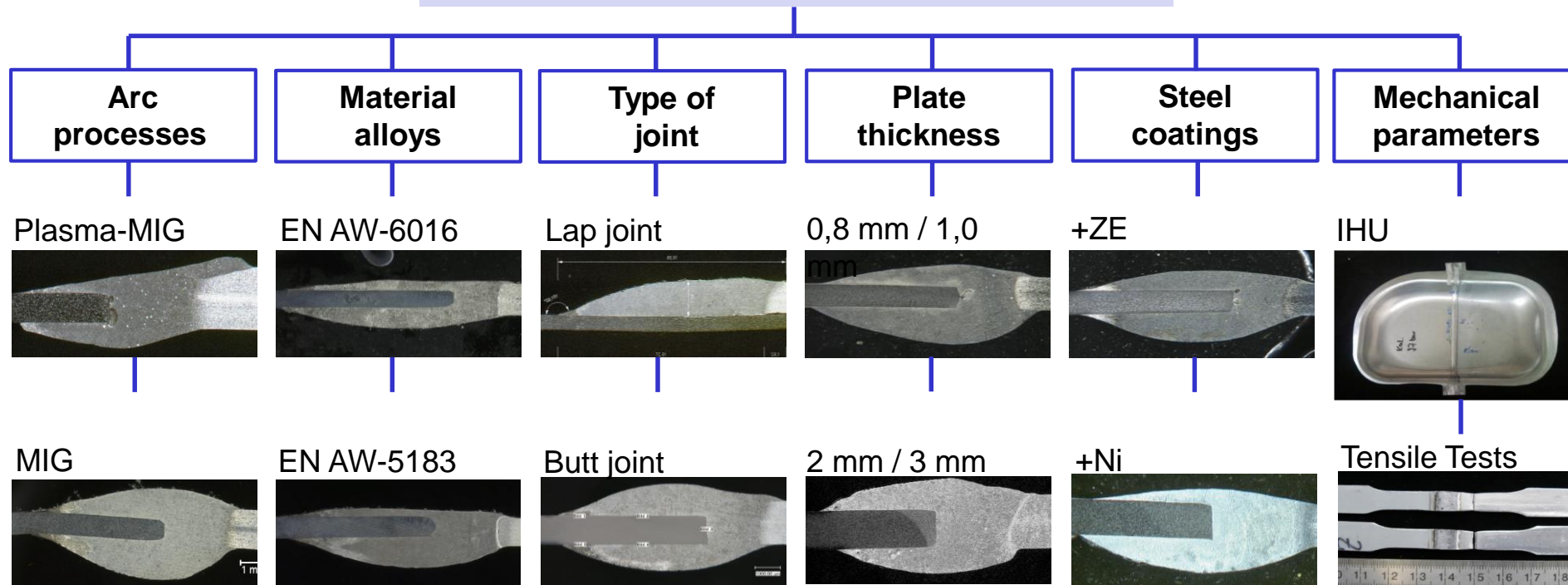
Source: Fronius



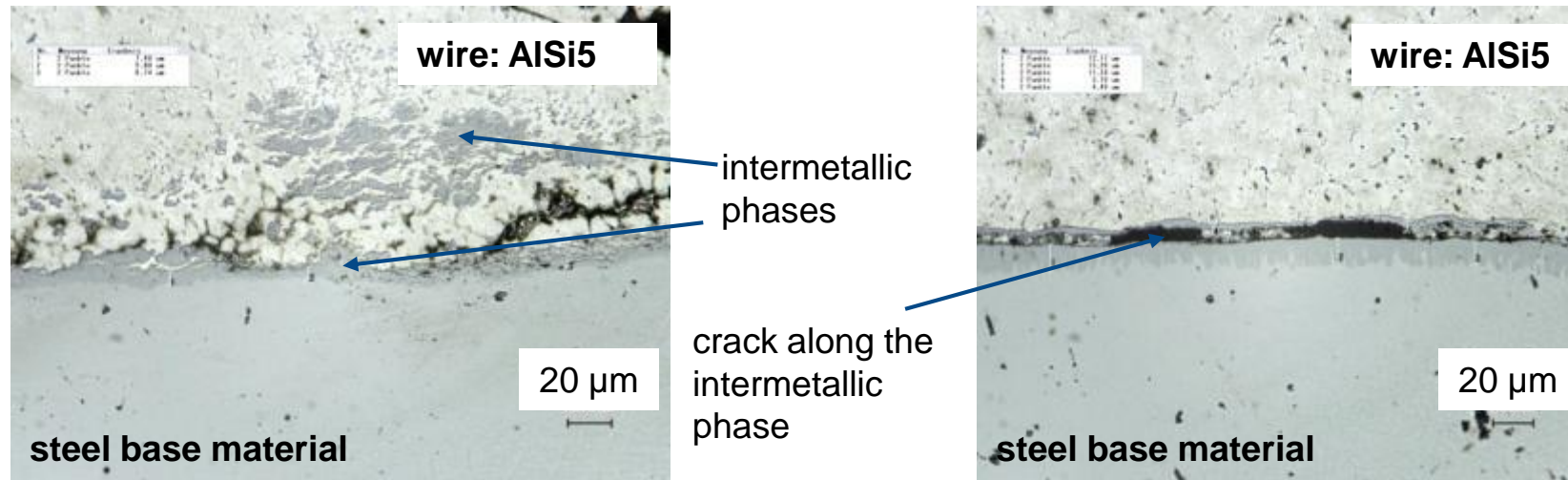
Steel-aluminium hybrid blank

Source: Voest-Alpine

Steel-Aluminum Dissimilar Material Joints



- During the last few years, several projects with the topic of joining steel with aluminum have been carried out.
- The focus of the research work has been put on the suitability of different aluminum filler materials (AlSi5, AlMg4,5Mn) for the joining of steel-aluminum dissimilar material joints.



- Formation of brittle intermetallic phases due to the non-existing solubility of steel and aluminum at room temperature. The phases must not exceed 10 µm.
 - Physical problems due to different melting points, expansion coefficients and thermal conductivity
 - Complex integration of the joining process into automobile production (application of flux, complex clamping devices due to distortion,
- ➔
- Compared with other thermal joining processes only small range of facility
 - Determination of the formation of the intermetallic phases is, so far, only possible by using destructive testing

Aims

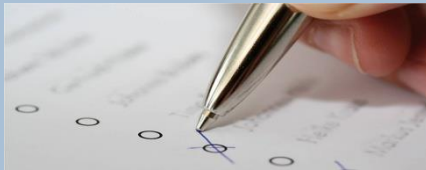


Joining of materials which are relevant in vehicle construction under practice-related boundary conditions

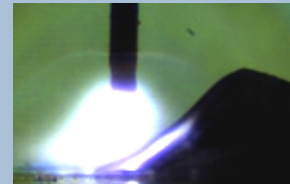


Reduction of the influence of the metallurgical incompatibility in thermal joining of steel and aluminum

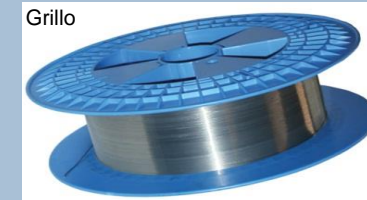
Approach



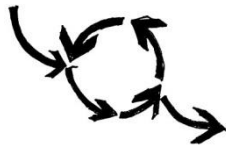
Testing of applications in vehicle construction by carrying out an assessment of demand



Lower energy input by the application of controlled short-arc processes (CMT, coldArc)

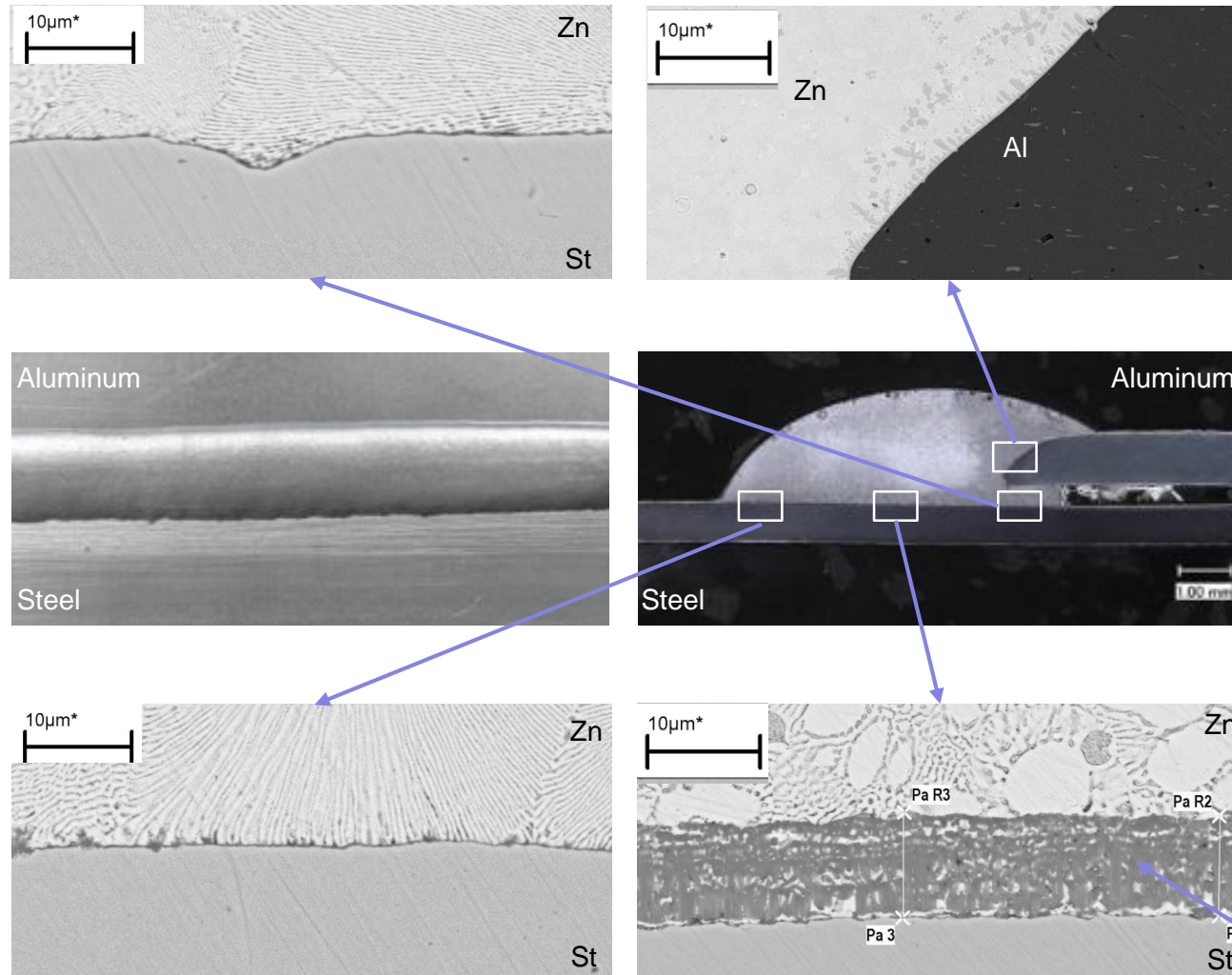


Further development of low melting zinc based brazing materials for application cases (alloying elements, diameter, surface condition, coating, etc...)



This development is carried out within the scope of iterative processes from the fields of users of vehicle construction (application know-how), welding institute (process know-how) and wire manufacturers (material know-how).

GRILLO



Application Case

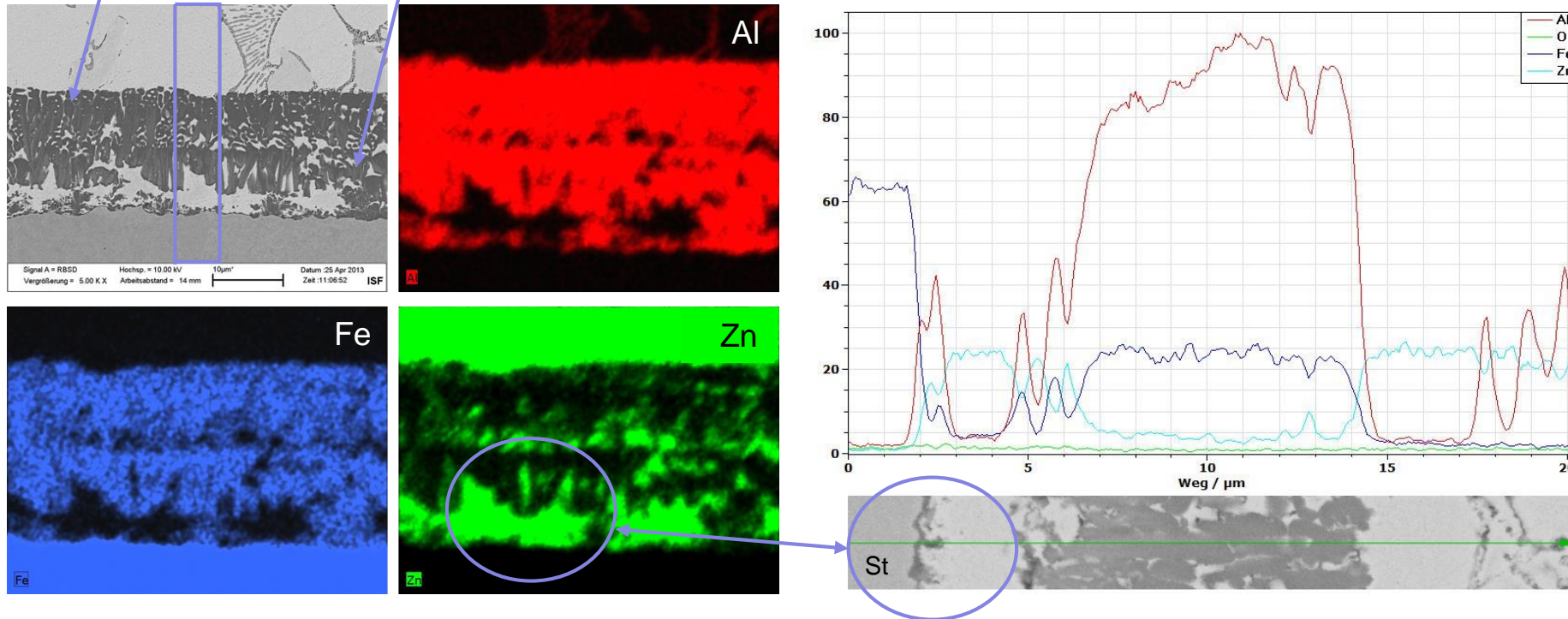
- Process-reliable joining of steel-aluminum dissimilar material joints without flux
- Development of weld geometries with mechano-technological favourable properties
- In the zone of the arc attachment point, a phase of steel, aluminum and zinc is developed which, compared with joining using an aluminum-based brazing material, is less brittle

Intermetallic phase which has been saturated with zinc (St/Al/Zn)

1st Phase

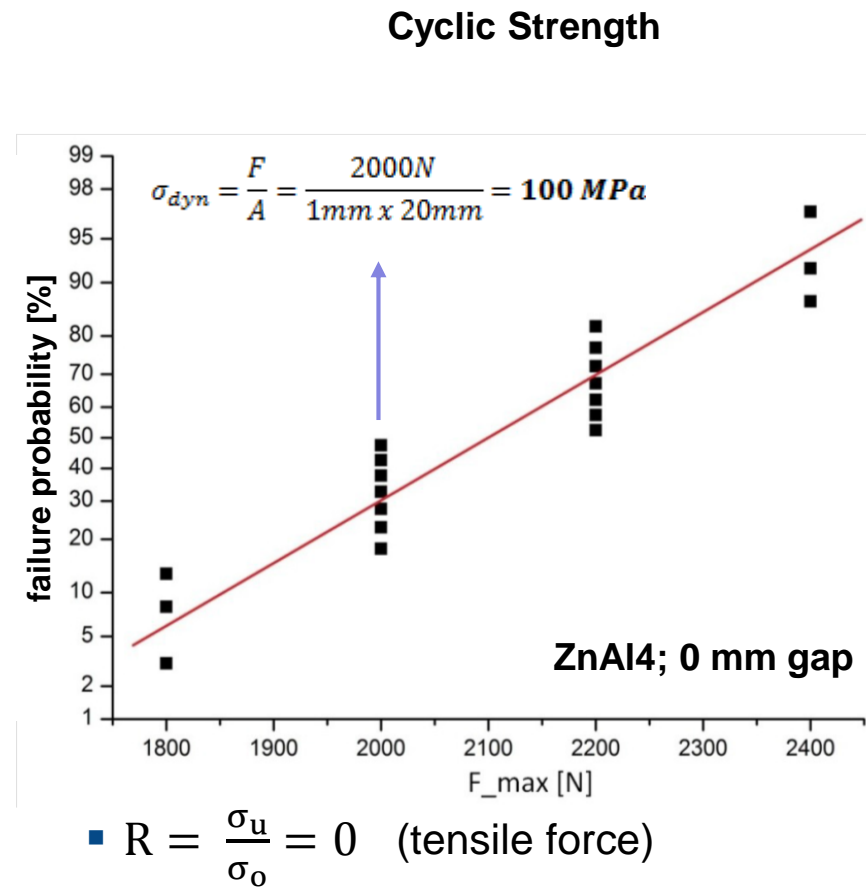
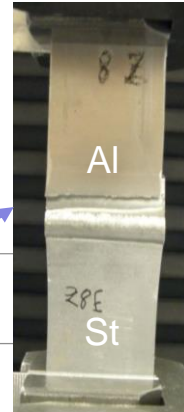
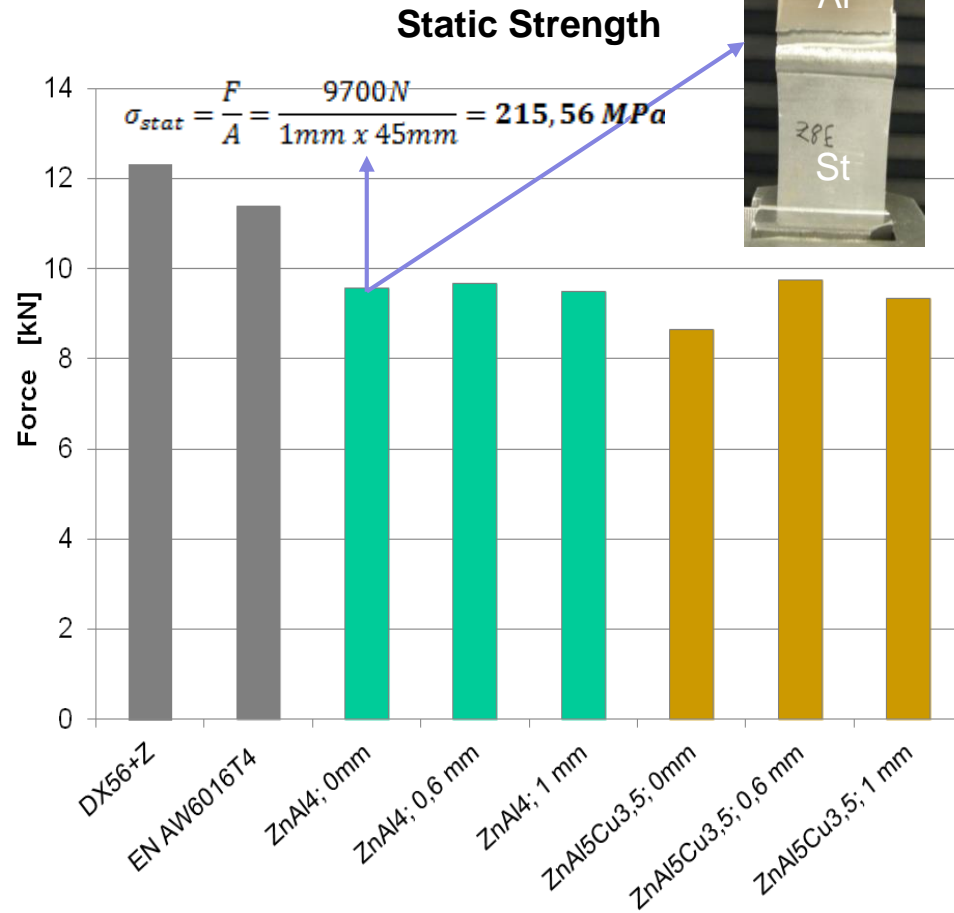
2nd Phase

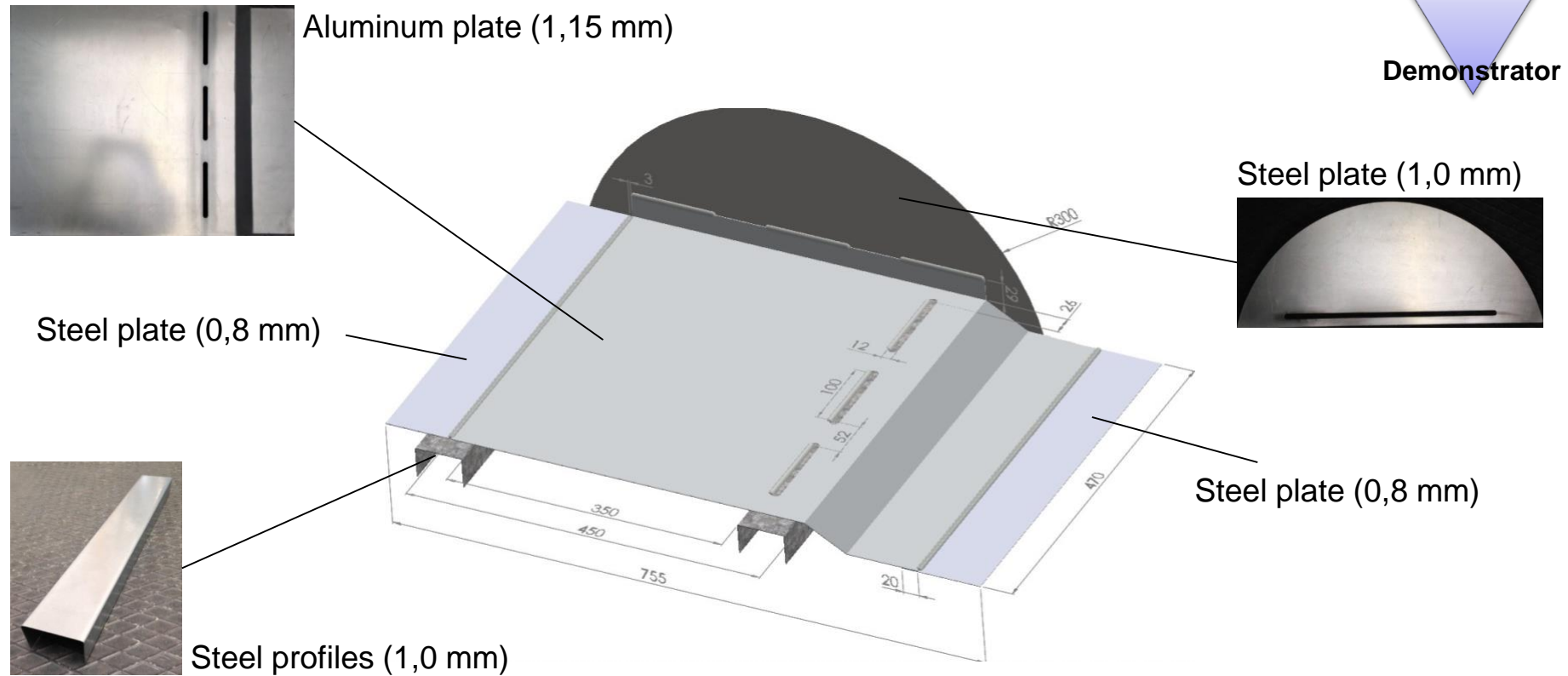
Application Case



- During the joining process, intermetallic phases are developed which detach as from a thickness of max. 5 μm and which are saturated by phases which are rich in zinc.
- A ductile phase which is rich in zinc is adjoining the steel base material.

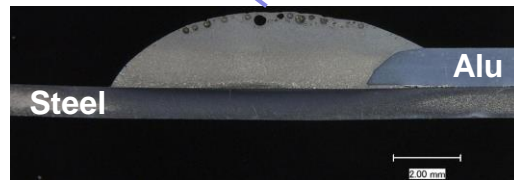
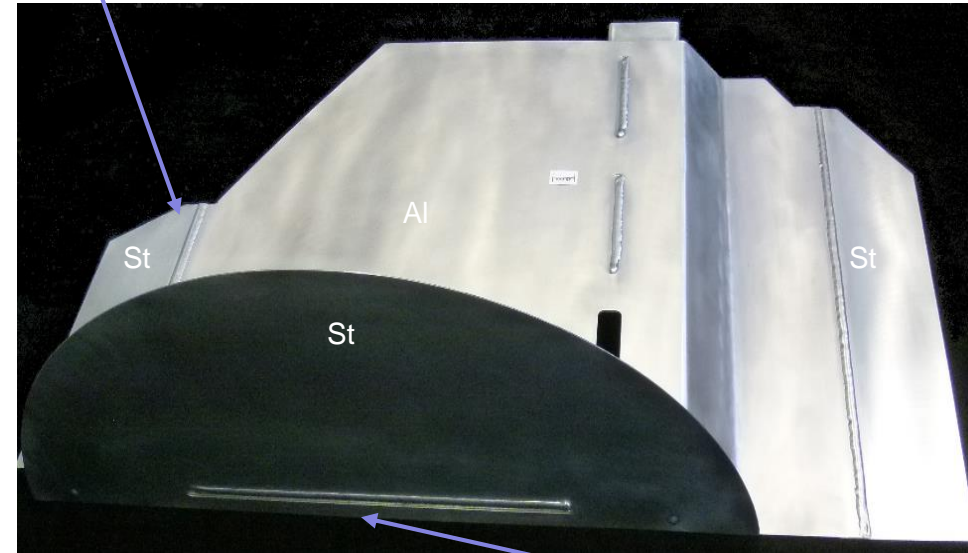
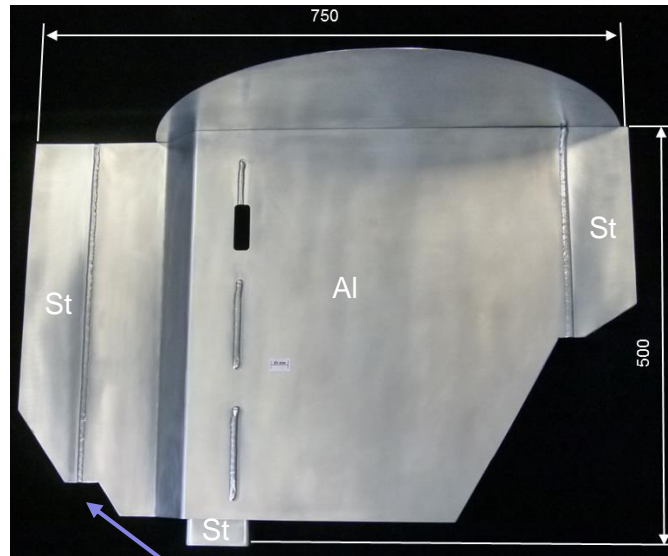
Application Case

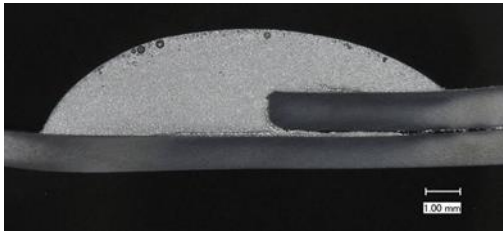




- The application of steel profiles and aluminum plates shall allow crash- and also lightweight relevant functions in a vehicle underbody.
- Demonstration of the possibility of joining different materials with different thickness and surface coatings.

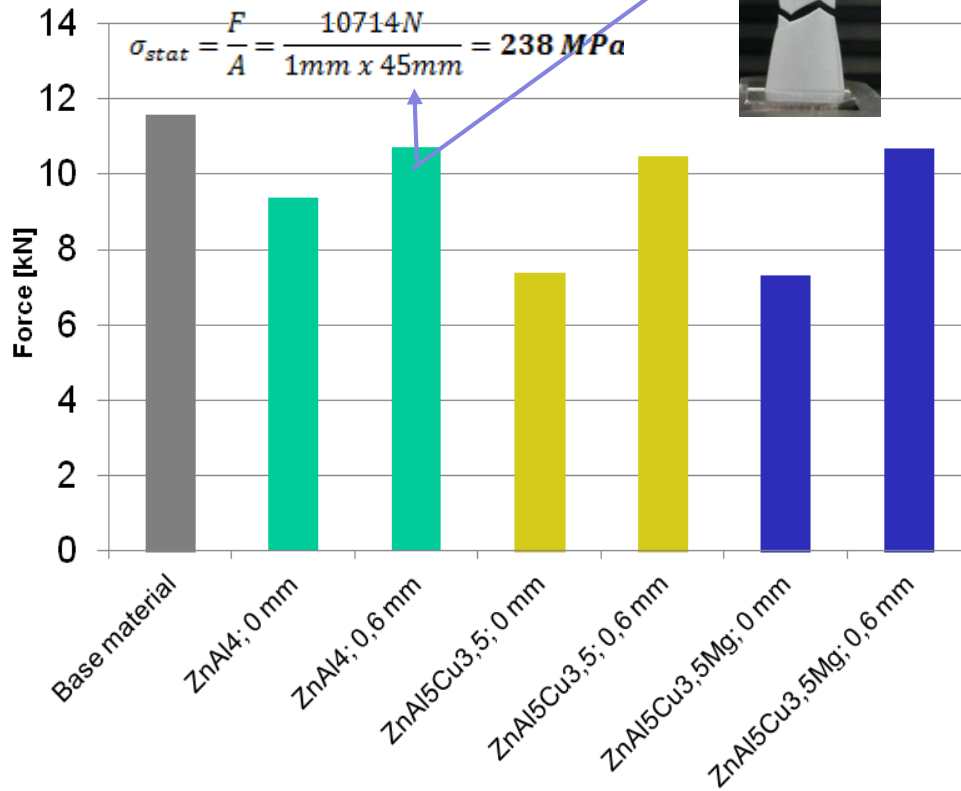
Demonstrator





Application Case

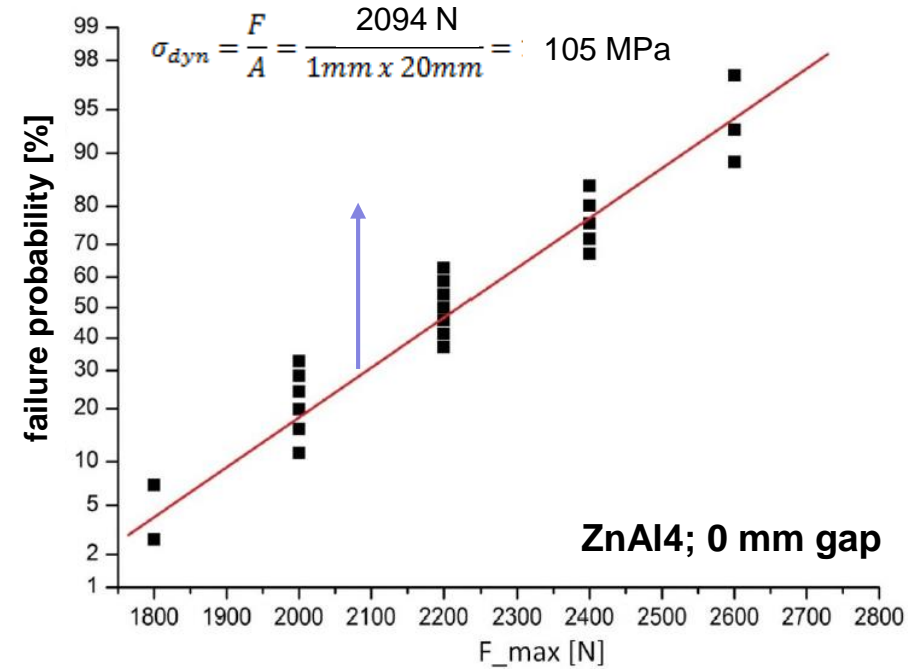
Static Strength



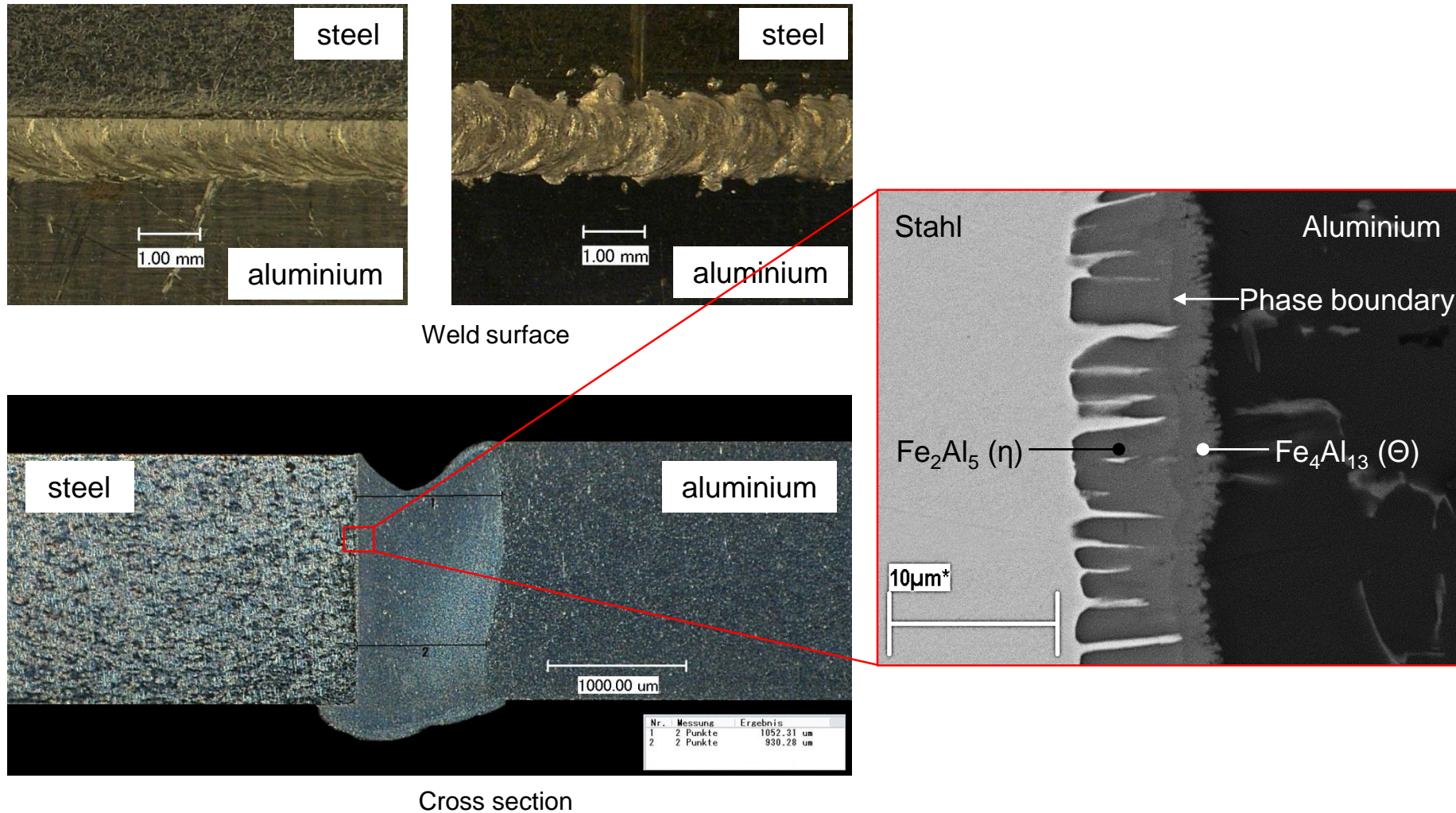
$$\sigma_{stat} = \frac{F}{A} = \frac{10714 N}{1 mm \times 45 mm} = 238 MPa$$

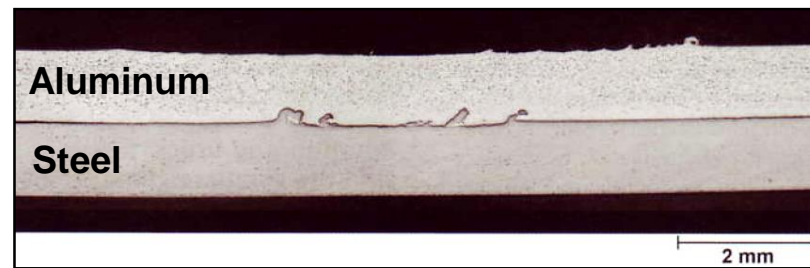
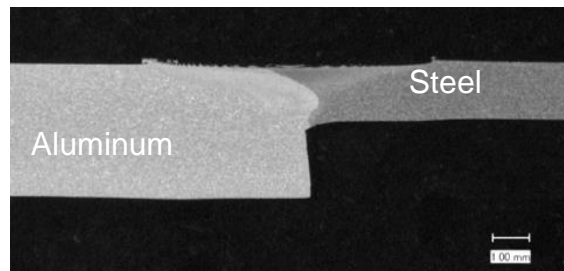
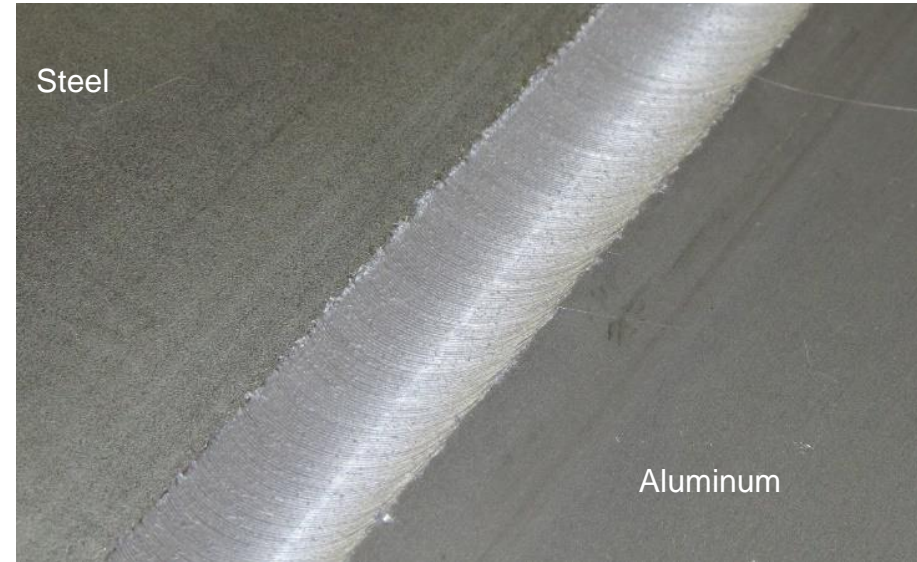
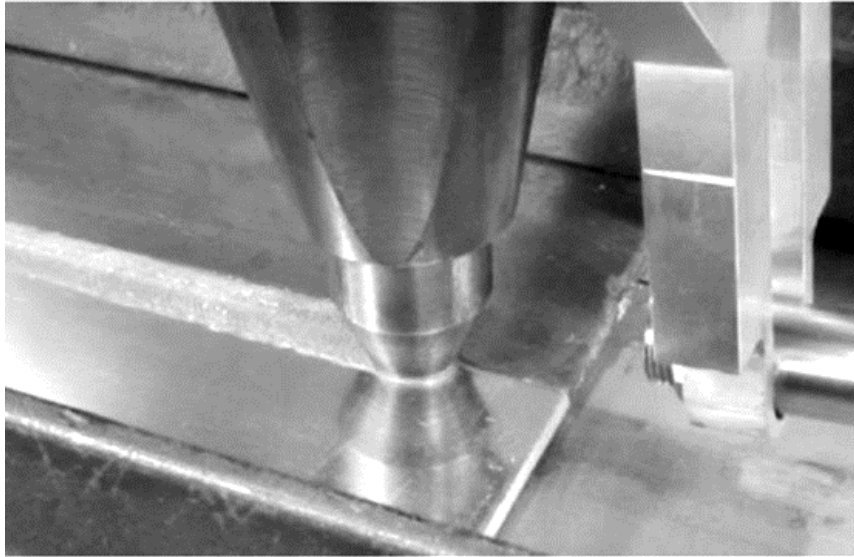


Cyclic Strength

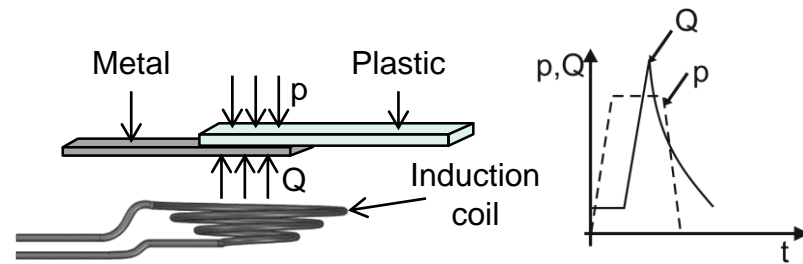


■ $R = \frac{\sigma_u}{\sigma_o} = 0$ (tensile force)

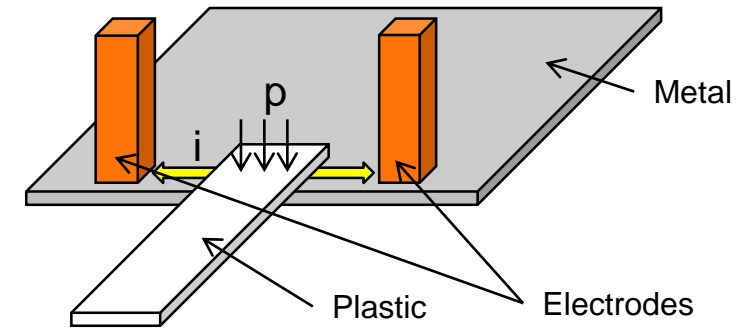




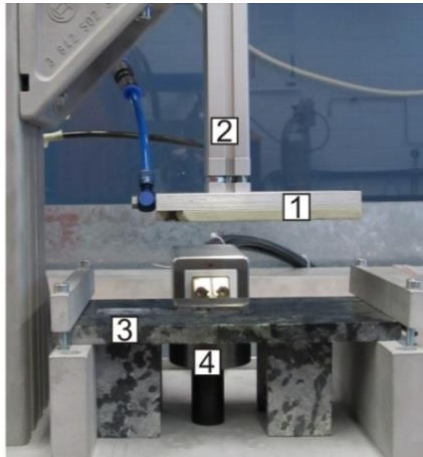
Principle induction technique



Principle resistance heating

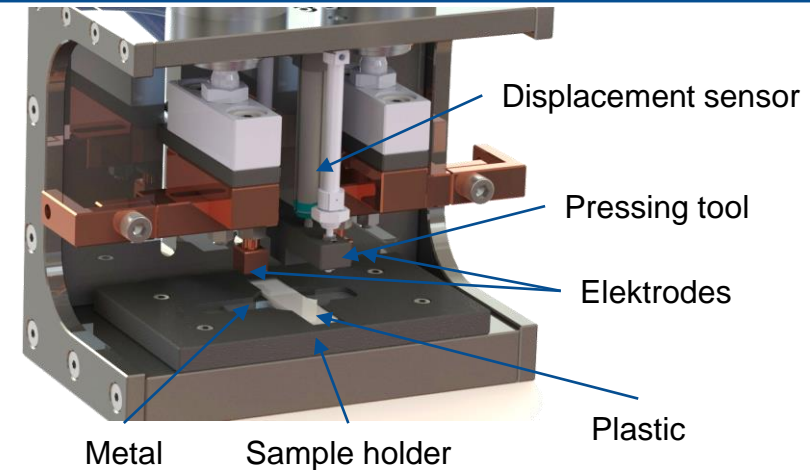


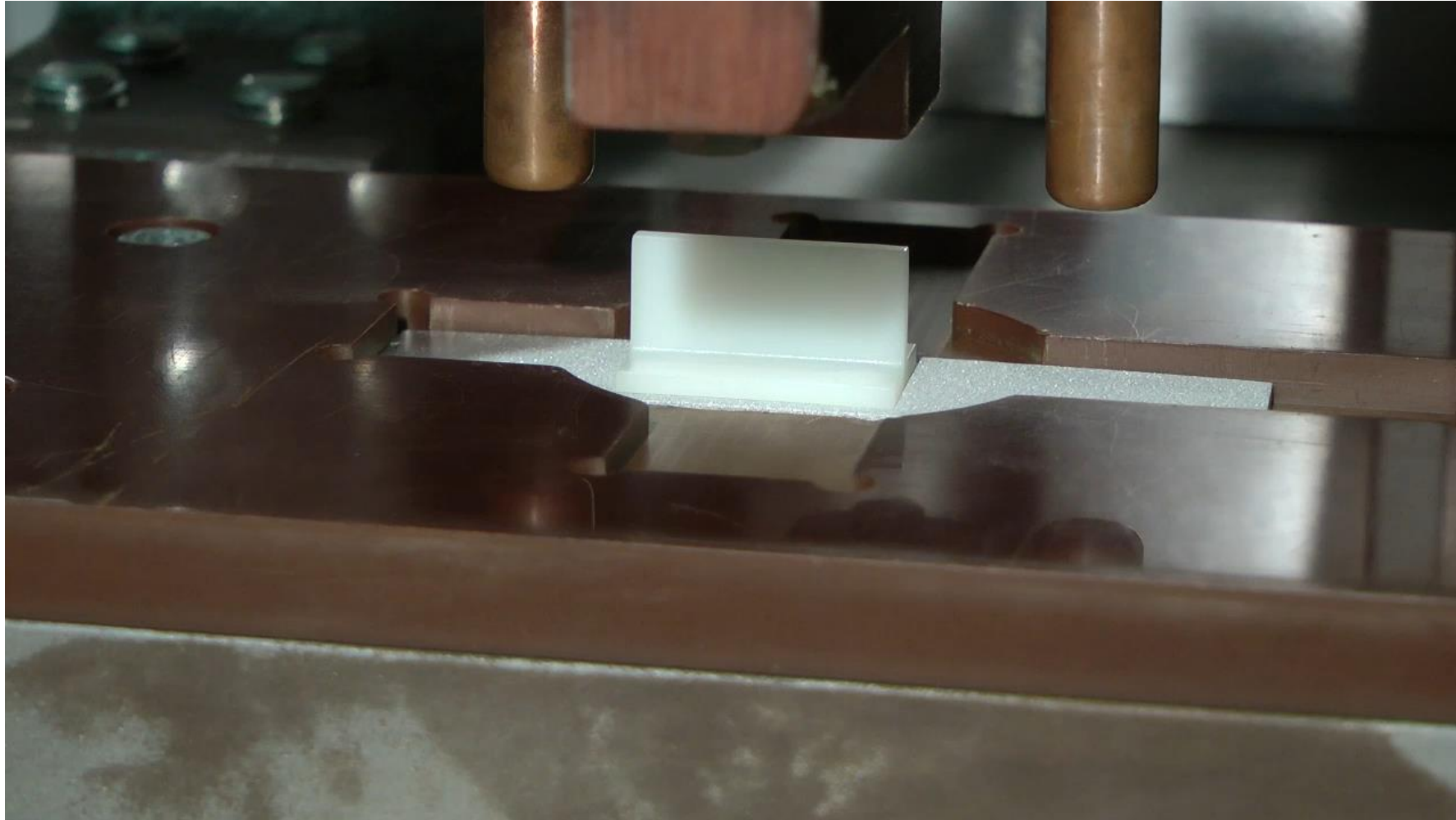
Experimental set-up induction technique



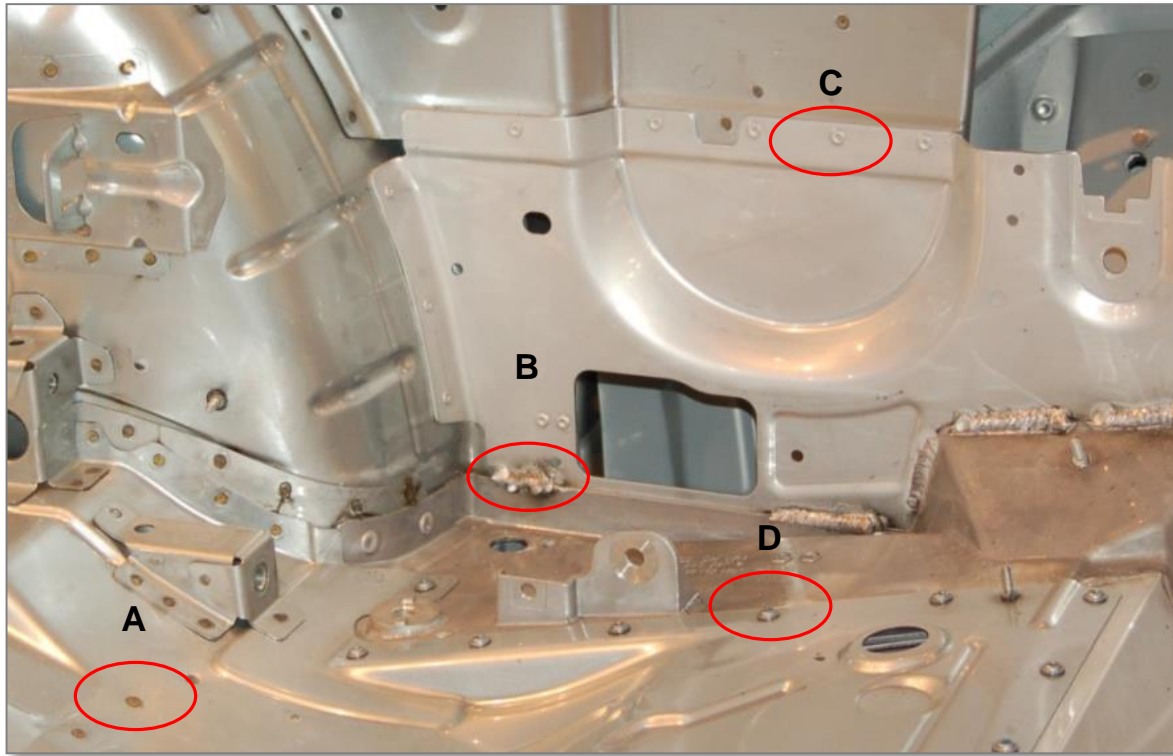
1. Upper sample holder (plastic part)
2. Pressing cylinder
3. Lower sample holder (metal part)
4. Induction coil

Experimental set-up resistance heating



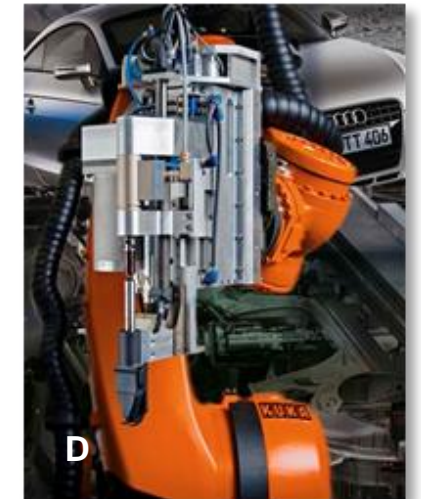
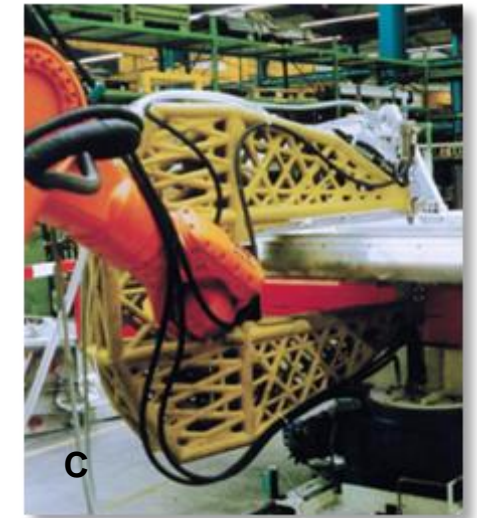
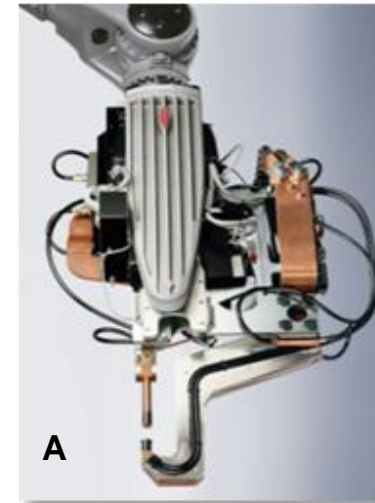


- Introduction
- Motivation
- Lightweight design and multi-material mix
- Challenges to joining technology
- **Composite design and multi-material mix in production**
- Summary



Audi TT, Source: Audi

- A:** Resistance spot welding
- B:** MIG welding
- C:** Rivetting
- D:** Flow-Drill Screwing





Technique	Process	Number per vehicle
Mechanical joining techniques	Rivetting	1615 piece
	Clinching	164 piece
	Flow-Drill-screwing	96 piece
	Solid rivetting	229 piece
Thermal joining techniques	MIG welding	21462 mm
	Laser welding	5309 mm
	RP welding	1287 spots
	MAG welding	809 mm
	Stud welding	234 piece
Adhesive bonding	Adhesive bonding	97156 mm

Source: DVS BV Schwaben, Franz J. Lange

Audi TT:

- 6 different wall thickness values
- 4 different rivet types
- 6 different materials Al
- 6 different materials St

Through the multi-material mix, the number of successor models has more than doubled

- Introduction
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- **Summary**

- Lightweight design is an important key for reducing the CO₂ emissions
- The singular steel-, aluminium and FVK (fibre reinforced plastic material) design is replaced by composite design and further by hybrid concepts
- New car body concepts pose new challenges to the joining technique
- Existing joining techniques are already capable to fulfill most of the joining tasks
- The current multi-material mix/composite design requires, as far as economic considerations are concerned, a very high number of joining technologies
- Economically speaking, the number of varieties within one joining technology is also too high
- Composite design requires joining techniques for a possibly large bandwidth of joining tasks